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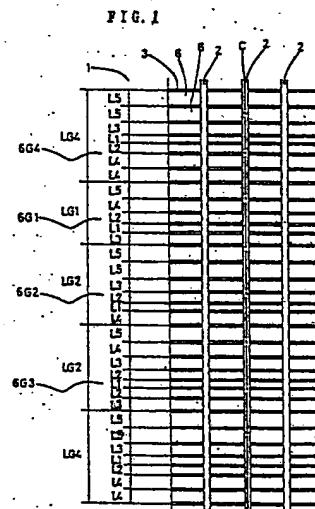
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A request for correction of the formula in the originally description has been filed pursuant to Rule 88 EPC. A decision on the request will be taken during the proceedings before the Examining Division (Guidelines for Examination In the EPO, A-V, 2.2).

㉖ Low noise tyre.

㉗ A low noise tyre which comprises a plurality of kinds of groups arranged in the circumferential direction and each formed in combination of a plurality of blocks having a circumferential pitch length  $L_i$  ( $i = 1, 2, 3, \dots$ , and so on in the order of the smaller pitch length). The block groups have three to five kinds of circumferential lengths  $L_{Gj}$  ( $j = 1, 2, 3, \dots$ , and so on in the order of the smaller circumferential length). Fifty five or more blocks are juxtaposed in the circumferential direction. The ratio  $P_i$  of the pitch lengths  $L_i$  ( $= L_i + 1/L_i$ ) of that two of the blocks, which are adjacent to each other in the order of the smaller length, is set at a value from 1.1 to 1.2. The ratio  $P_{max}$  ( $= L_{max}/L_1$ ) of the maximum pitch length  $L_{max}$  of the blocks to the minimum pitch length  $L_1$  is set at a value from 1.5 to 1.9.

EP 0 268 436 A2



## Description

LOW NOISE TYRE

The present invention relates to a low noise tyre.

5 In block pattern tyres in which the tread pattern is formed by blocks separated by longitudinal and transverse grooves, air is discharged from and sucked into the grooves as a result of compressions and expansions of the grooves as a result of rolling of the tyre on a road surface. The discharges and suction cause repeated noises. Further noises include pattern noises or impact noises accompanied by compression waves in the ambient air. These also are caused by the repeated pulsating vibrations generated by the blocks. These noises may also be of the same frequency as resonant frequencies of individual portions of the vehicle and thus be amplified into the vehicle.

10 In order to reduce these noises, a variable pitch method is known in the art, in which the pitch length of the blocks, i.e. the minimum wave unit of the repeated tread pattern, is varied so as to spread the noises themselves over a broad frequency spectrum thereby to drop the peak noise level and to avoid high peaks in the noises from being further increased by resonance in the noise frequency.

15 According to this variable pitch method, however, several kinds of blocks having different pitch lengths are arranged in the circumferential direction of the tyre. If the ratio of the longest pitch to the shortest pitch is excessive a circumferential imbalance is liable to occur in the rigidity of the tread so that the vibratory characteristics during rolling of the tyre are adversely affected and cause eccentric wear in the tyre. If the pitch arrangement is regular, however, the result is that the noises are uncomfortable to the ears.

20 It is, therefore, an object of the present invention to provide a low noise tyre by selecting the number of blocks, the ratio of the pitch lengths of the blocks and the number of the kinds of block groups thereby to disperse the tyre noises over a broad frequency range and give effectively white noise and at the same time avoid the problem of eccentric wear.

25 According to the present invention, there is provided a low noise tyre comprising a plurality of kinds of groups arranged in the circumferential direction and each formed in combination of a plurality of blocks having a circumferential pitch length  $L_i$  ( $i = 1, 2, 3, \dots$ , and so on in the order of the smaller pitch length), wherein the improvement resides: in that said blocks groups have three to five kinds of circumferential lengths  $L_{Gj}$  ( $j = 1, 2, 3, \dots$ , and so on in the order of the smaller circumferential length); in that fifty five or more of said blocks are juxtaposed in the circumferential direction; in that the ratio  $P_i$  of the pitch lengths  $L_i$  ( $= L_{max} + 1/L_i$ ) of that two of said blocks, which are adjacent to each other in the order of the smaller length, is set at a value from 1.1 to 1.2; and in that the ratio  $P_{max}$  ( $= L_{max}/L_1$ ) of the maximum pitch length  $L_{max}$  of said blocks to the minimum pitch length  $L_1$  is set at a value from 1.5 to 1.9.

30 Other objects, features and advantages of the present invention will become apparent from the following description of one embodiment by way of example only, described with reference to the accompanying drawings, in which:

Fig.1. is a laid out plan view showing a portion of the tread pattern according to one embodiment of the present invention;

Fig.2. is a diagram showing the arrangement of the blocks of the tread pattern and their groups;

Fig.3. is a diagram for explaining the block groups;

40 Fig.4. is a graph showing the number of blocks and peak noise level index;

Fig.5. is a graph for explaining the relationship among the pitch length ratio of the blocks, the number of kinds and the peak level index;

Fig.6. is a spectrum showing the result of frequency analysis for the case in which block groups with variable circumferential length are used;

45 Fig.7. is a spectrum showing the result of frequency analysis for the case in which block groups with equal circumferential length are used;

Fig.8. is a spectrum showing frequency analysis values of the noises of the embodiment of the present invention; and

50 Fig.9. is a spectrum showing the frequency analysis values of the noises of a prior art tyre for comparison.

In Fig.1 a tread 1 is formed by three longitudinal grooves 2 extending in the circumferential direction of the tyre to define ribs, and transverse grooves 3 extending through the ribs in the axial direction of the tyre to form blocks 6 arranged in rows. The central longitudinal groove 2 extends along the equator line C of the tyre. Thus sixty five or more blocks 6 are juxtaposed for each rib around the whole circumference of the tyre.

55 As shown in Fig.4, the peak noise level index of the pitch noises generated for each block 6 reduces with increasing block number N. If the block number N exceeds 65 the degree of dispersion improvement reduces, as shown, towards a minimum level.

The peak noise level is a satisfactory fraction such as 30 if the number N is fifty five or more. It was therefore decided that the block number N should be fifty five or more, or more preferably sixty five or more.

60 Here, the aforementioned peak noise level index is defined as follows: If the highest sound pressure of the one-dimensional component of the pattern noises which are generated by the tyre tread pattern (i.e. single-pitch pattern) arranged with blocks of equal length around the whole tyre circumference, is 100, the peak noise level index expresses in percentage terms the ratio of that highest sound pressure to that of the

one-dimensional component of the pattern noises which are generated by the variable length block tyre tread pattern (e.g.) irregular pitch pattern). The peak noise level index thus defined is calculated by the method of simulating the degree of dispersion of pitch noises through a harmonic analysis in which the arrangements of the blocks with different lengths on the tyre circumference are represented by pulse trains. The maximum of  $1Hn$  calculated by the following equation is defined as the peak noise level index

$$|H_n| = |Co \sum_{k=1}^N w_k \cdot e^{j \cdot 2\pi y/L_T \cdot x_k}|$$

wherein:

$|H_n|$ : an harmonic component of  $n$ -th order

$Co$ : a normalisation constant for  $H_n = 100$  at  $n$ -single pitch;

$w_k$ : a pulse weighing constant;

$L_T$ : a circumferential length of tyre

$N$  the total number of blocks; and

$x_k$ : the position of  $K$ -th pulse.

In the embodiment the aforementioned blocks 6 are composed of five kinds of circumferential pitch lengths  $L_i$ . In the tyre tread, moreover, there are juxtaposed in the circumferential direction block groups  $6G_j$  which have circumferential lengths  $LG_j$  (wherein  $j = 1, 2, 3, \dots$ , and so on in the order of smaller length first) in combination of several blocks 6.

Incidentally, the pitch length  $L_i$  of the blocks 6 is the circumferential length between the centres of the transverse grooves 3 and 3 dividing said blocks 6, and these comprise different pitch lengths  $L_i$  ( $i = 1, 2, 3, 4$  and 5), as has been described above. Note that the reference characters  $i = 1$  to 5 are arranged in the order of the smaller pitch length first. Furthermore the ratio  $P_i (= L_i + 1/L_i)$  of the pitch length  $L_i$  of the first block of the smallest length, is set at a value from 1.1 to 1.2. The ratio  $P_{max}$  of the maximum pitch length  $L_{max}$ , i.e.  $L_5$  to the minimum pitch length  $L_1$  of the blocks 6 is set at a value from 1.6 to 1.9.

As shown in Fig.5, even if the aforementioned pitch ratio  $P_i$  is set at 1.10, the peak noise level index  $\varepsilon$  can be set at 30 or less by increasing the kinds of the pitch  $L_i$  of the blocks 6 to 5 or more. Therefore, the number of kinds of the pitch length  $L_i$  is set at 5 or more. If the number of kinds is 15 or more, however, tyre production is troublesome.

Moreover, the ratio  $P_i$  of the pitch length  $L_i$  of the blocks adjoining in the order of the smaller lengths is set at the aforementioned value from 1.1 to 1.2. If the ratio  $P_i$  is smaller than 1.1, as is apparent from Fig.5, the reduction in the peak noise level index  $\varepsilon$  is not sufficient even when the number of the pitch lengths  $L_i$  of the blocks 6 is five. If the ratio  $P_i$  is larger than 1.2, on the other hand, the difference in the length among the blocks becomes too large to allow the rigidity balance around the tyre tread to be reasonable and eccentric wear of the tyre is caused, thus spoiling the other performance requirements for the tyre.

If the ratio  $P_{max}$  of the maximum pitch length  $L_5$  to the minimum pitch length  $L_1$  exceeds 1.9, the one- and two-dimensional components of the pitches of the noise frequency may overlap and this then increases the noise level. As has been described above, therefore, the ratio  $P_{max}$  of the pitch length has its upper limit set at 1.9.

If the ratio  $P_{max}$  of the pitch length is the biquadrate of 1.1, i.e. about 1.46, if the number of kinds of the pitch length  $P_i$  is 5 and if the ratio  $P_i$  of the pitch length is 1.1 or more then, the ratio  $P_{max}$  has its lower limit set at 1.5 or more, as has been described above.

Moreover, the aforementioned block group  $6G_j$  ( $j = 1, 2, 3, \dots$ , and so on) is composed of three to five kinds of circumferential lengths  $LG_j$  ( $j = 1, 2, 3, \dots$ , and so on in the order of the smaller length). The embodiment shown in Figs.1 and 2 includes four kinds of block groups  $6G_1$ ,  $6G_3$  and  $6G_4$ . On the other hand, the ratio  $PG_j (= LG_j + 1/LG_j)$  of the block group  $6G_j$  to the circumferential length  $LG_j$  is set at the value from 1.1 to 1.5. Moreover, the ratio  $PG_{max}$  of the maximum circumferential length  $LG_{max}$ , i.e.  $LG_4$  to the minimum circumferential length  $LG_1$ , is set at the value from 1.5 to 1.9.

Incidentally in the present embodiment, the block groups  $6G_4$ ,  $6G_1$ ,  $6G_2$  and  $6G_3$  having the circumferential lengths  $LG_4$ ,  $LG_1$ ,  $LG_2$  and  $LG_3$  are repetitively arranged in the rected order in the circumferential direction, as shown in Figs. 1 and 2.

Here, the block group  $6G_j$  is defined, if the aforementioned blocks 6 of five different circumferential lengths  $L_i$  are arranged at random in the circumferential direction of the tyre, as that from the block 6 with the maximum circumferential length  $L_5$  (or the block with the smallest pitch length  $L_1$ ) to the block 6 with the next maximum circumferential length  $L_5$  (or the block 6 with the smallest pitch length  $L_1$ ). On the other hand, the length between the centres of the transverse groove 3 and 3 in the circumferential direction of the tyre is specified as the circumferential length  $LG_j$  ( $j = 1, 2, 3, \dots$ , and so on in the order of the smaller circumferential length) of the block groups  $6G_j$ . Incidentally, an abnormal interruption such as a block 6A with the maximum circumferential length  $LG_5$ , for example, in one block group  $6G_j$ , as shown in Fig.3, is ignored.

Incidentally, the number of the blocks 6 in each block group  $6G_j$  can be freely set. In the embodiment of Figs.1 and 2, moreover, the blocks groups  $LG_1$  and  $LG_4$  contain five, six or seven blocks 6 with respectively different lengths.

Incidentally the blocks can be set to form the whole circumference of the tyre by arranging each of the aforementioned block groups 6G1 to 6G4 in the circumferential direction of the tyre. In this instance, the number of the blocks 6 contained in each block group 6Gj becomes large.

Moreover, it has been found that the so-called "wow" noises are caused which offend the ears if the block group is of less than three kinds whereas the peak noise level index drops if the block group is of more than five kinds. In the present embodiment, therefore, there are used the block groups 6G1 to 6G4 having four circumferential lengths LG1 to LG4. Still further the ratio PGj ( $= LGj + 1/LGj$ ) of the circumferential length LGj of the block group 6Gj is set at a value from 1.2 to 1.5, as has been described above.

If the circumferential lengths LGj of the block groups 6Gj are identical, prominent peak noises are liable to occur in the one- and two-component dispersion widths of the pitches in the noise frequency, as shown in Fig.7, to drop the peak noise level index  $\epsilon$ . If the circumferential lengths LGj are made variable, on the contrary, both the one- and two-components can be dispersed to a satisfactory extent, as shown in Fig.6, to change the noise into white ones.

It has also been found as the result of investigations that the peak noise level index  $\epsilon$  is large if the aforementioned ratio PGj of the circumferential lengths is smaller than 1.2 whereas the length difference becomes excessive to rather drop the peak noise level index  $\epsilon$  if the ratio PGj exceeds 1.5.

However, the ratio PGmax, i.e. PG4 of the maximum circumferential length LGmax, i.e. LG4 to the minimum circumferential length LG1 has to be more than the square of 1.2, i.e. more than 1.5 because the aforementioned ratio PGi of the circumferential length LGi is 1.2 or more.

If the aforementioned ratio PGi of the circumferential lengths LGi exceeds 2.5, moreover, the ratio of the block lengths becomes excessive to make it liable to separate and discriminate the noises of long or short periodic pitch so that the noises are prevented from becoming white noise. Therefore, the ratio of the circumferential lengths and the maximum and minimum values are set at the above specified values.

Incidentally, in the embodiment shown in Fig.1, each block is formed to have the same phase in the circumferential direction for each rib. Despite this fact, however, it is possible to further improve the white noise generation by changing the phase of each block in the circumferential direction.

One specific example will now be described which is a tyre having the size of 185/60R14 and a block pattern as Fig.1 was manufactured with the specifications enumerated in the column of Table 1.

Another tyre having the specifications enumerated in the right hand column was also manufactured for trial by way of comparison. These two tyres were subjected to noise spectrum analysis. The noise measurements were performed by a rotating drum test, and the tyres were rotated under a load near that of service and at a running speed of 50 km/hour. The results of noise measurements of the embodiment are shown in Fig.8, and those of the comparison are shown in Fig.9. These results reveal that the noises in the embodiment of the present invention were spread over a broad frequency spectrum and turned into white noise so that the resultant perceived pattern noise was reduced.

The tyre of the present invention was virtually the same in steering stability and wear resistance to the comparison tyre.

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	COMPARISON	EMBODIMENT
Number of Blocks	65	65
Number of Kinds of Block Pitch Length	3	5
Pi	1.15 1.15	1.15 1.15 1.15 1.15
Pmax	1.32	1.75
Number of Kinds of Circumferential Lengths of Block Groups	3	4
PGi	1.4 1.4	1.3 1.3 1.3
PGmax	1.96	2.20

Thus by selecting the kinds of the block pitch lengths, the ratio of the lengths, and the number of kinds of block groups each composed of the blocks according to this invention a lower noise tyre is obtained which disperses the noises over a broad frequency range thereby to change them into white noise so that the offending noises of the tyre can be reduced to improve the comfort of the vehicle in relation to noise levels.

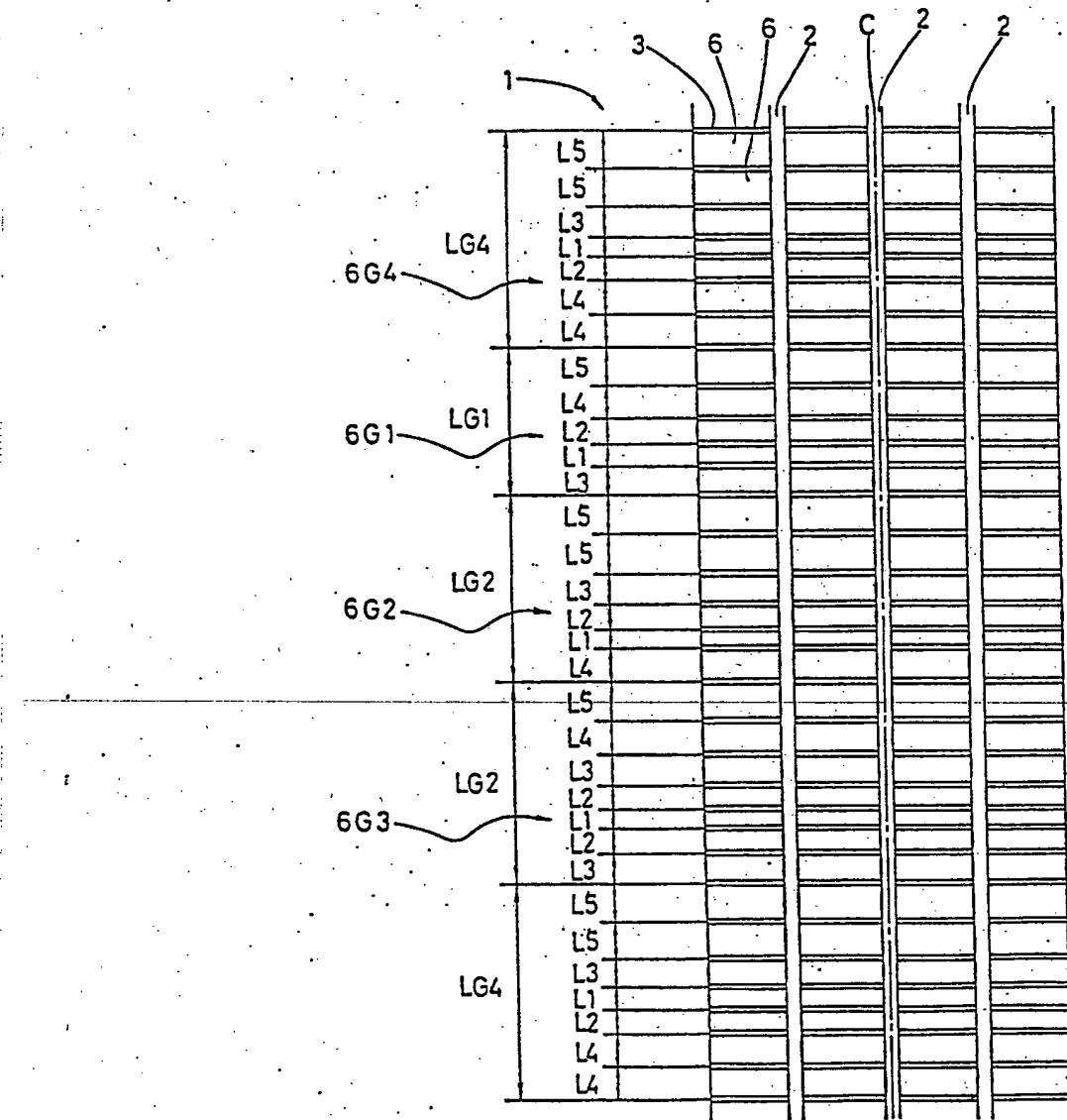
#### Claims

1. A low noise tyre comprising a plurality of kinds of groups arranged in the circumferential direction and each formed in combination of a plurality of blocks having a circumferential pitch length  $L_i$  ( $i = 1, 2, 3, \dots$  and so on in the order of the smaller pitch length), characterised in that the said block groups have three to five kinds of circumferential lengths ( $L_{Gj}$  ( $j = 1, 2, 3, \dots$ , and so on in the order of the smaller circumferential length first) fifty five or more of said blocks are juxtaposed in the circumferential direction; the ratio  $Pi$  of the pitch lengths  $L_i$  ( $= L_i + 1/L_i$ ) of that two of said blocks, which are adjacent to each other in the order of the smaller length, is set at a value from 1.1 to 1.2; and the ratio  $Pmax$  ( $= Kmax/L1$ ) of the maximum pitch length  $Lmax$  of said blocks to the minimum pitch length  $L1$  is set at a value from 1.5 to 1.9.

2. A low noise tyre according to claim 1, characterised in that the ratio  $PGj$  ( $= PGj + 1/PGj$ ) of the circumferential length  $L_{Gj}$  of the block groups adjacent in the order of said smaller length is set at a value from 1.2 to 1.5, and the ratio  $PGmax$  ( $= LGmax/LG1$ ) of the maximum circumferential length  $LGmax$  to the minimum circumferential length  $LG1$  is set at a value from 1.5 to 2.5.

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FIG. 1



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FIG. 2

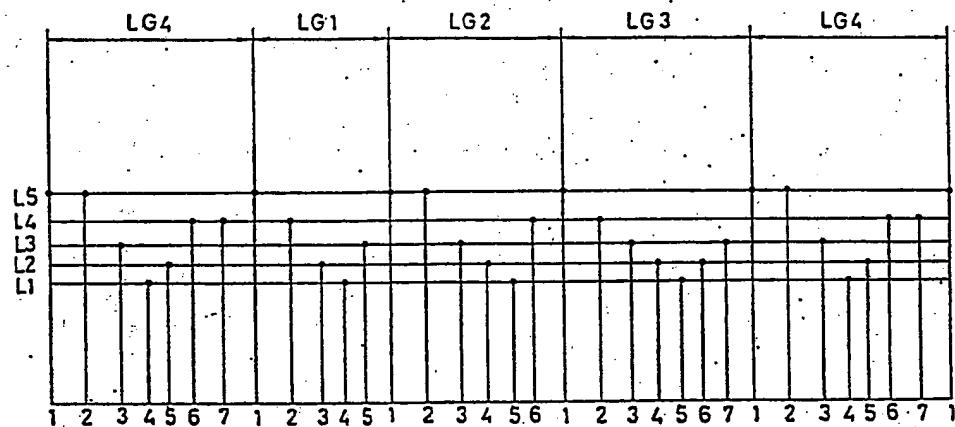
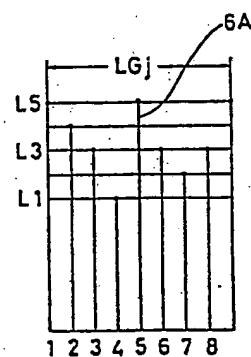


FIG. 3



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FIG. 4

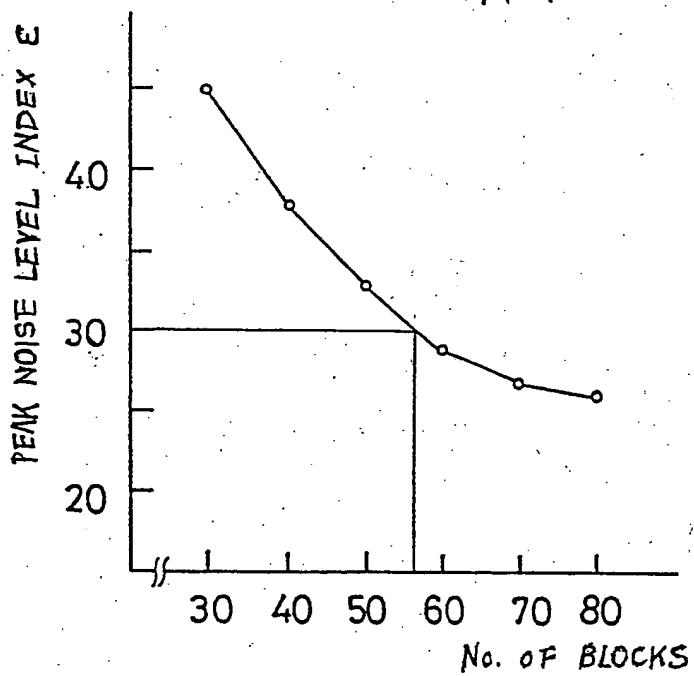
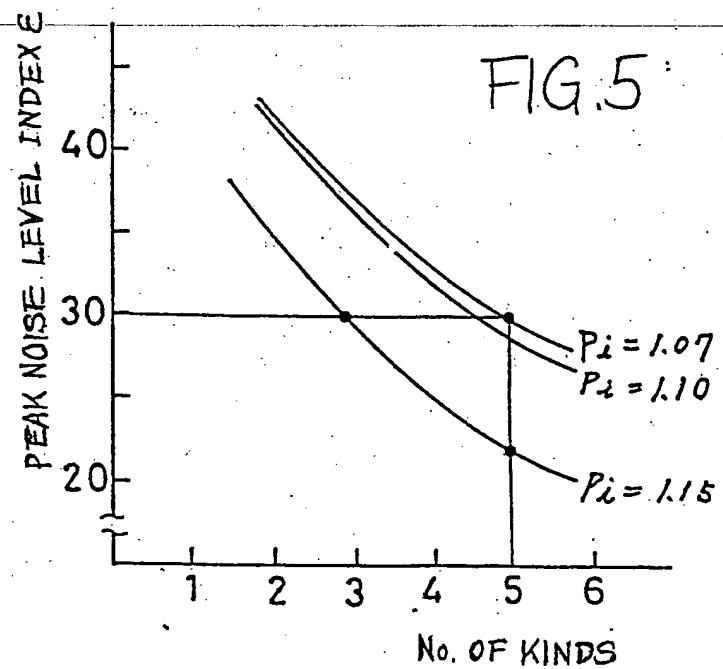


FIG. 5



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FIG.6

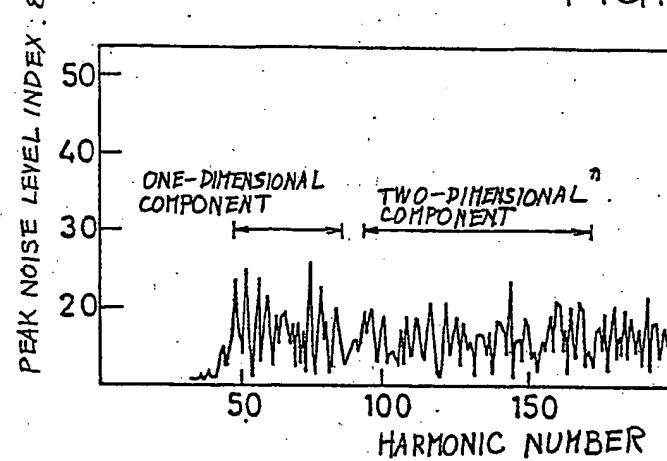
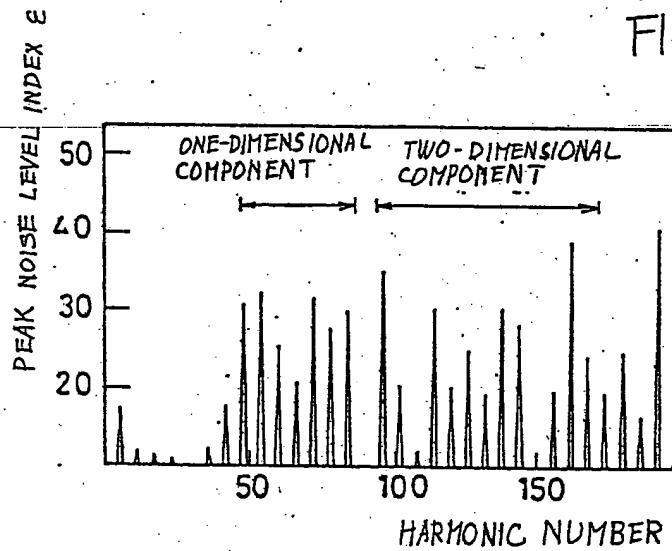


FIG.7



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FIG. 8

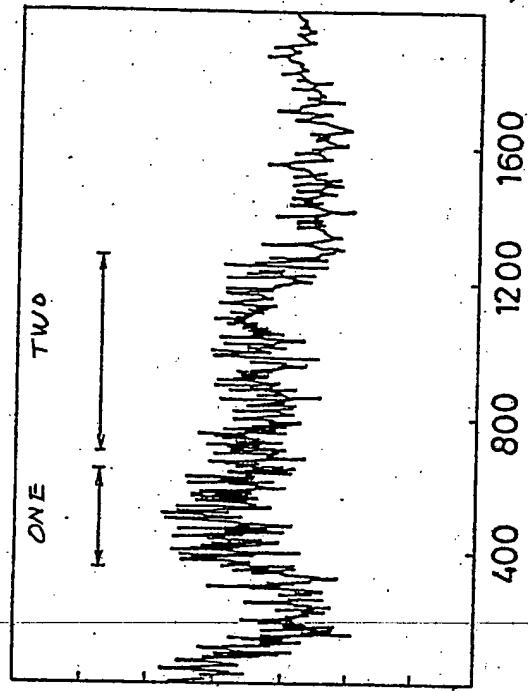


FIG. 9

